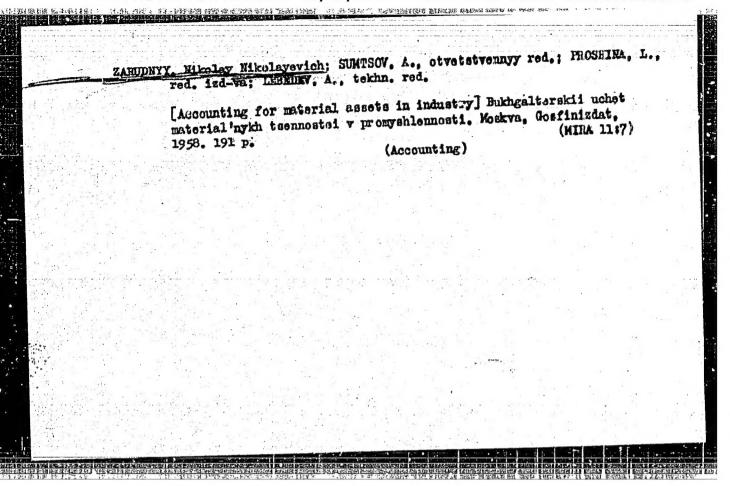
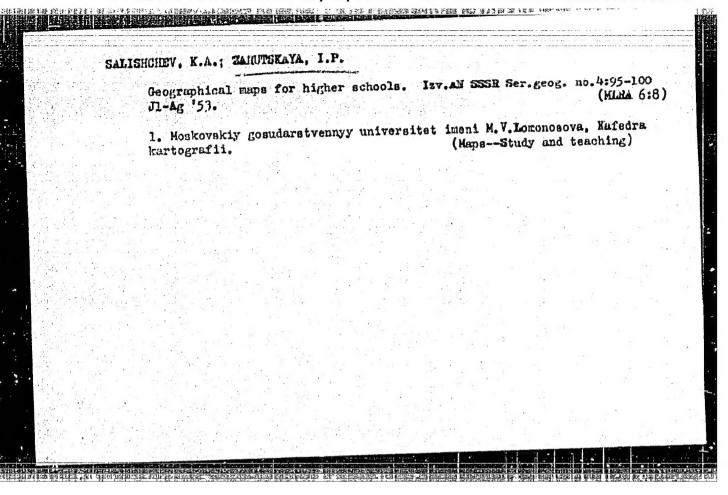
TITOV, Kohstantiatir Markovich; ZARUDNYY, N.N., otv. red.; MAZURKEVICH, M., red. izd-va; LEREDEV, A., tekhn. red.

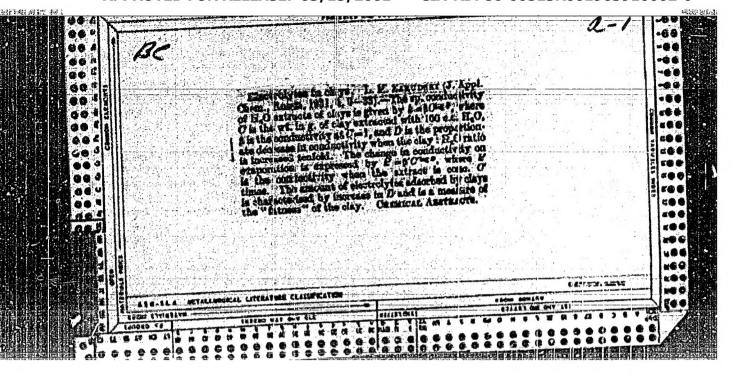
[Accounting for the clearing and credit operations of enterprises]

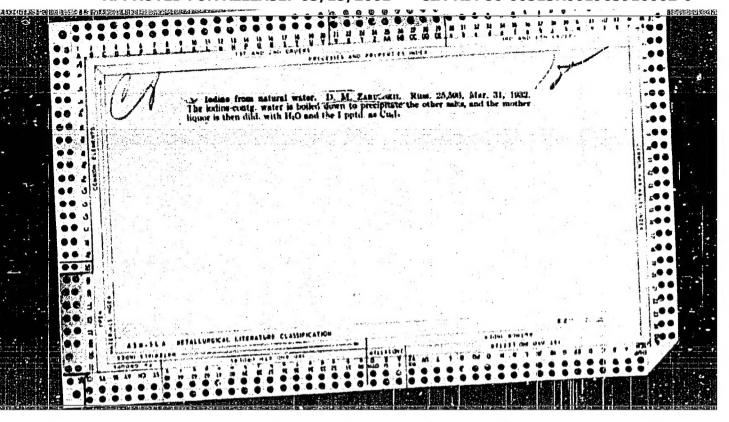
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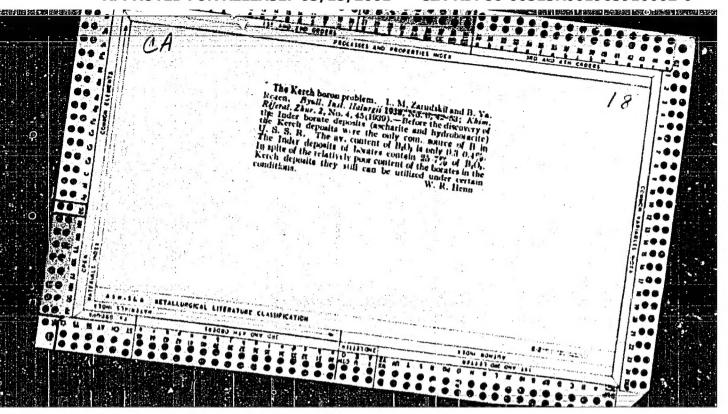
(Eanks and banking—Accounting) (Clearinghouse)

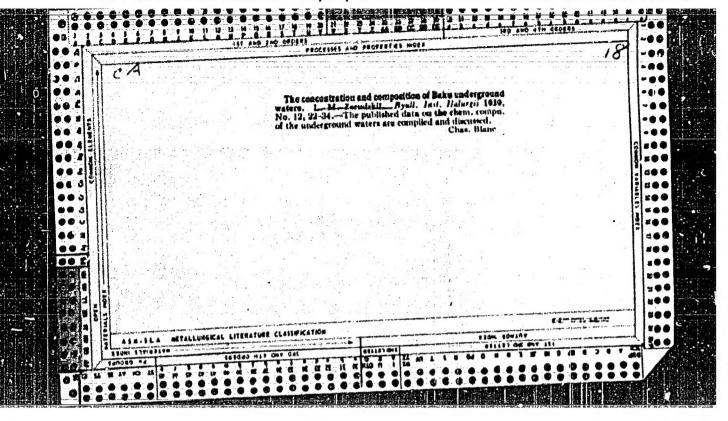


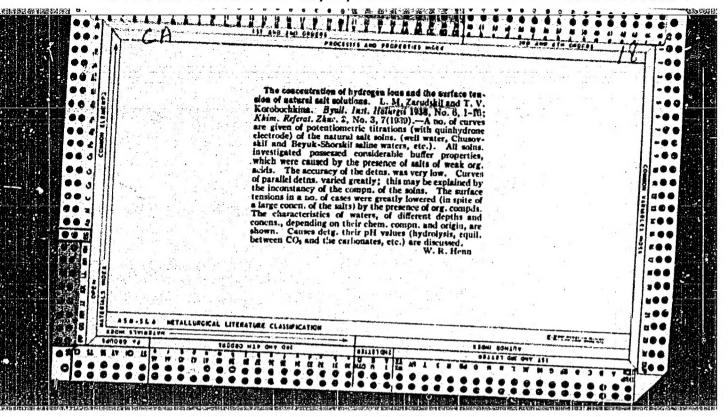


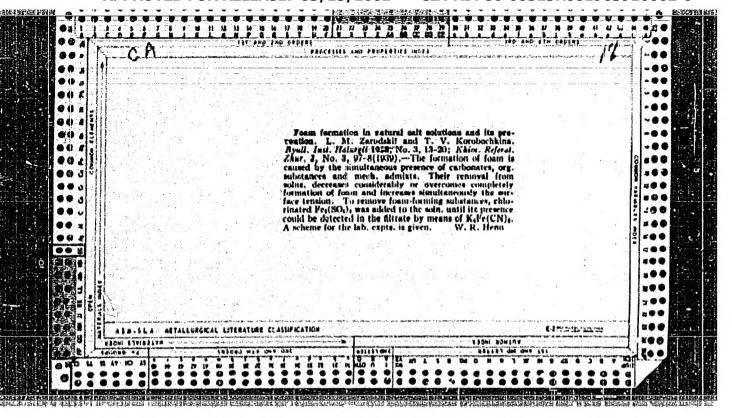


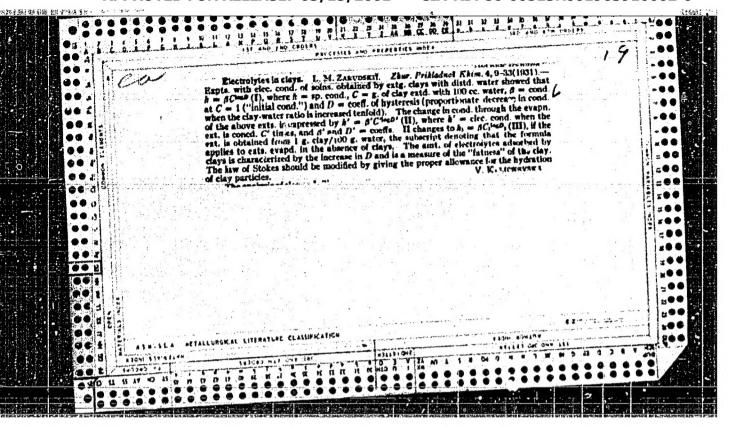








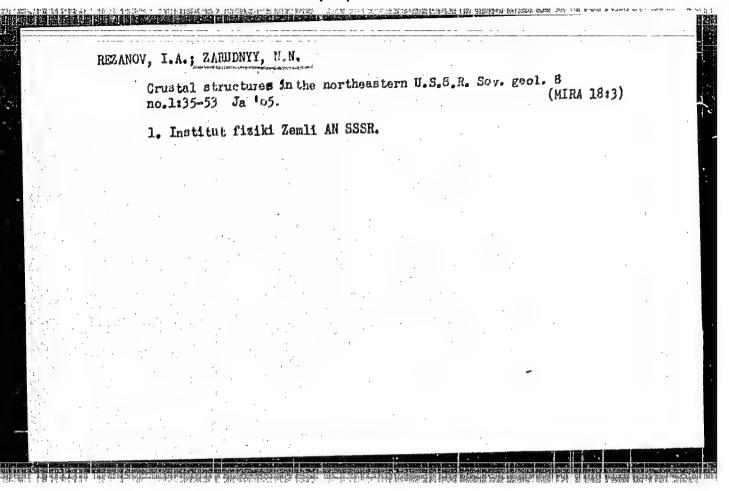




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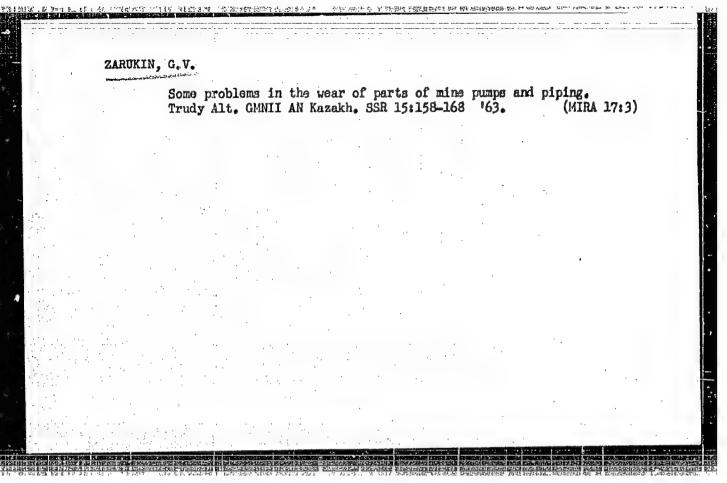


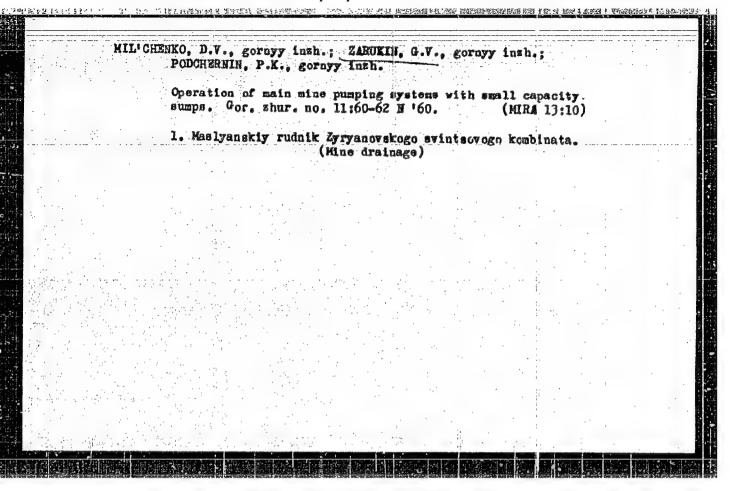
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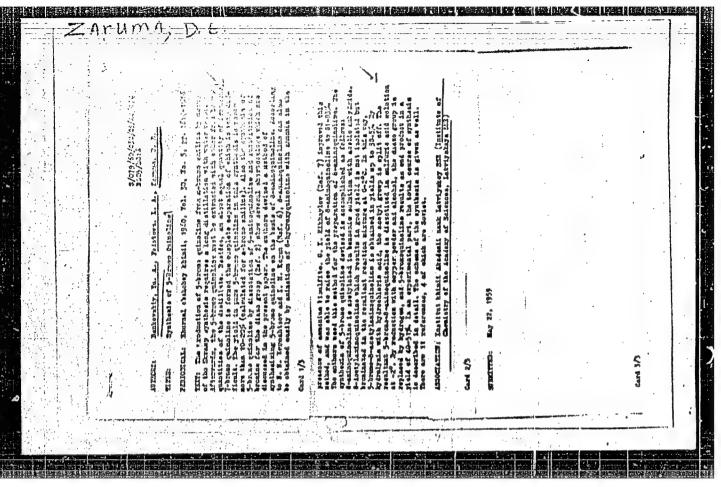
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Vol. 31, No. 7, July 1955
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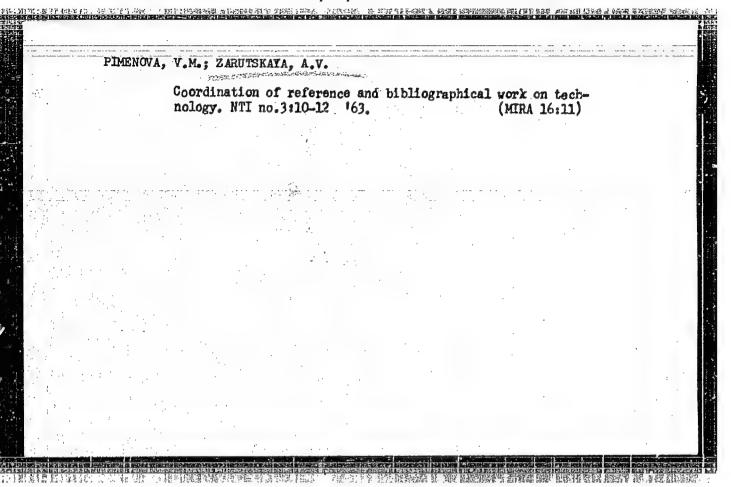


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1. Institut khimii Akademii nauk Latviyekoy SSR.

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"Hypsometric Map of USSR," I. P. Zarutskaya
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"Geographical Maps for Higher Schools," a paper given at the All-University Scientific Conference "Lomonosov Lectures", Vest. Mosk. Un., "o.S, 1953.

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3(4)

PHASE I BOOK EXPLOITATION

SOV/2017

Zarutskaya, Irina Pavlovna

Metody sostavleniya rel'yefa na gipsometricheskikh kartakh (Methods of Compiling Relief on Hypsometric Maps) Moscow, Geodezizdat, 1958. 214 p. Errata slip inserted. 3,000 copies printed.

Ed.: V.S. Volynskaya; Ed. of Publishing House: T.A. Shamarova; Tech. Ed.: M.V. Botvinko.

PURPOSE: This book is intended for cartographers, geographers, and teachers of mapping courses in vuzes and tekhnikums.

COVERAGE: The entire text, with minor exceptions, is devoted to problems of proper relief portrayal on hypsometric maps. A history of early hypsometric maps and the development of the hypsometric method in Soviet cartography is given in the first two chapters. General problems of compiling and editing hypsometric maps are discussed in detail. A chapter is devoted to the treatment of

Card 1/5

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Methods of Compiling Relief (Cont.) special relief features such as plains of denudation and me graphic representation is explained. There are 136 reference of which are Soviet, 9 English, 4 German, and 2 French.	ountain ed topo-	21
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	Special characteristics of portraying some types of mountain and plateau relief	13
	Special characteristics of portraying some types of flatland relief	13
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	Generalization processes performed during editing and preparatory work Selection of individual details in the process of map compilation	172
	Graphic construction of generalized relief representation.	188
	Clarifying notes and numerical (contour) indicators in religeneralization	199 ief
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Plan of the new series of special maps of world natural conditions and resources. Vop.geog. no.42:126-138 | 58. (MIRI 11:11) (Physical geography--Maps)

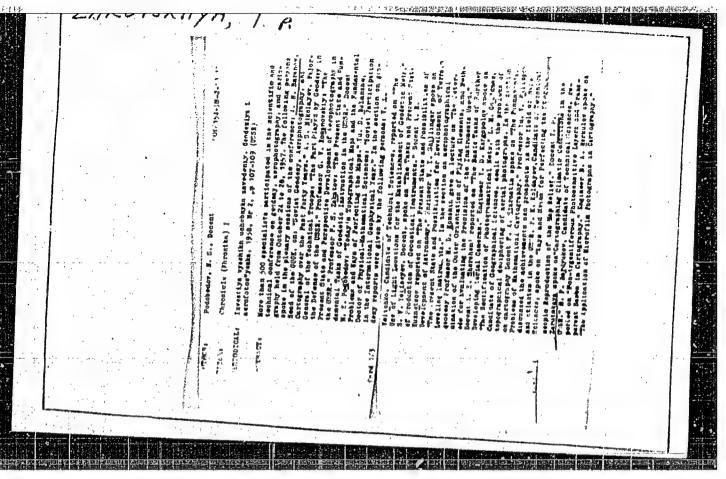
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RSFSR (for Tutochkina). 3. Chleny-korrespondenty AN SSSR (for Lavrenko,
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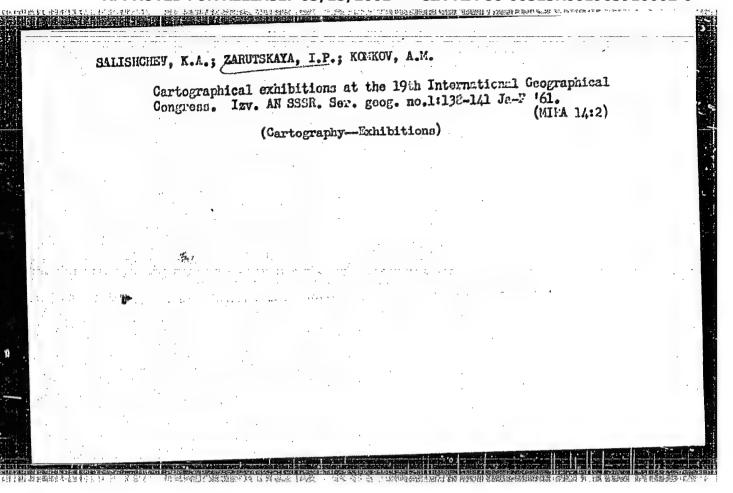
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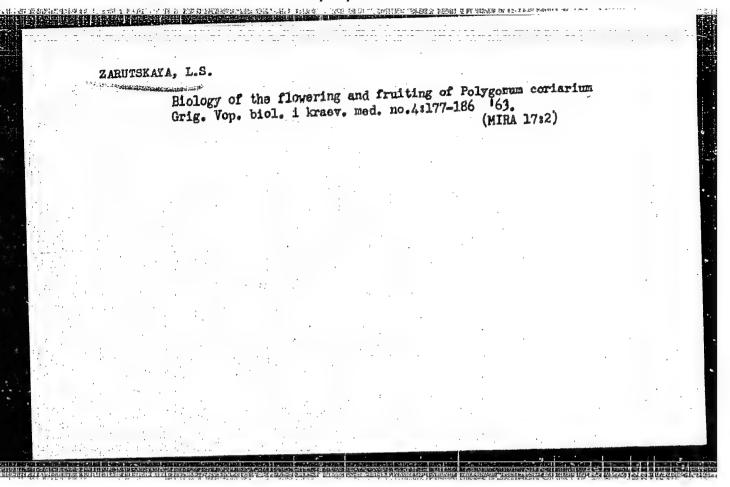
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The outstanding Soviet cartographer Konstantin Alekseevich
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Z ARUTSKAYA, V. C. ZARUTSKAYA, V. G. USSR/Medicine - Dysentery

FD_13

Card 1/1

Authors

*Ravich-Birger, Ye. D. and Zarutskaya, V. G.

Title

Data concerning the investigation of the Sonne bacillus. I. Microbio-

logical characteristics of Sonne dysentery microorganisms

Periodical

Zhur. mikrobiol. epid. i immun. 4, 40-45, Apr 1954

Abstract

This is the first in a series of 3 reports on the Sonne dysentery bacillus. It discusses the microbiological characteristics of 2 types of colonies formed by Sonne dysentery bacilli, i.e. a round form and a flat form. It shows that, although these 2 forms are morphologically distinct, their fermentative activity, virulence, and toxicity are almost identical. It indicate, the value of these characteristics in diagnosis and in the identif at on of the Sonne bacilli. The report is illustrated by 4 photographs and the results of the microbiological investigations are presented in 3 graphs. No references are cited.

Institution :

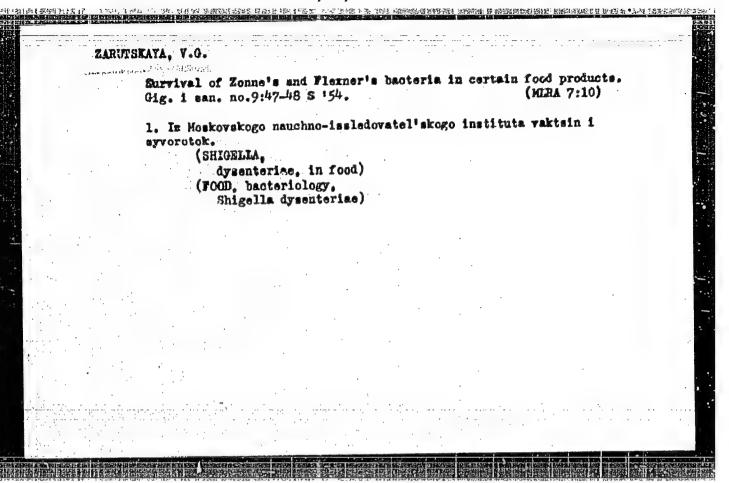
Moscow Scientific-Research Institute of Vaccines and Serums (Director - M. G. Kashtanova, Scientific Head V. A. Chernokhvostov, Head of the

Division of Intestinal Infections - *Ye. D. Ravich-Birger)

Submitted

July 3, 1953

ZARUTSKAYA, V. G.: Master Med Sci (diss) -- "The distribution and methods of detecting dysentery microbes in the external environment". Moscow, 1959. 12 pp (Min Health USSR, Central Inst for the Advanced Training of Physicians), 200 copies (KL, No 11, 1959, 122)



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	1. Iz Moskovsko logii, mikrobio voditel'-prof. Birger) (AGAR, raus	ologii i gig V.A.Chernokl	ivanv (dir.M	i.G. Kasntun	OAN" NERGURAL	uko-		
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[Theory of analytic functions of several complex variables]
Teoriia analiticheskikh funktaii mnoglikh kompleksnykh peremennykh. Izd.2., perer. i dop. Moskva, Fizmdegis.
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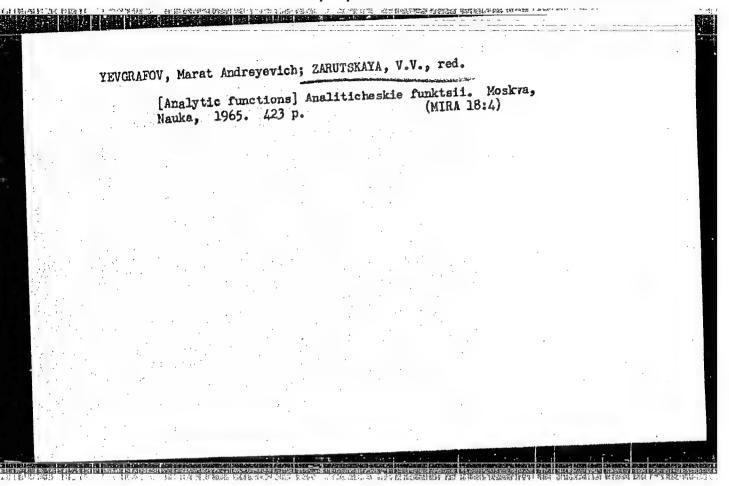
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1. Die Eidgenössische Technische Hochschule in Edrich (for
Butiskhauzer).

(Algorism) (Electronic calculating machines)



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ZARUTSKIY, Ivan Pavlovich; KONDRAT'YEV, Yu.P., red.; ALABYSHEVA, N.A., red.izd-va; GVIRTS, V.L., tekhn. red.

[Mechan.zation of lost-wax molding processes] Mekhanizatsiia izgotovleniia litia po vyplavliaemym modeliam. Leningrad, 1963. 18 p. (Leningradskii dom nauchnotekhnicheskoi propagendy. Obmen peredovym opytom. Seriia: Liteinoe proizvodstvo, no.4) (MIRA 17:4)

ZARUTSKIY. K.M. [Zaruts'kyi, K.M.]

Relief of the bed of the Pre-Quaternary sedimentary cover of the right bank of the middle Dnieper Valley. Do. AN URSR no.5:649-652 (64.)

1. Institut geologicheskikh pauk AN UkrSSR. Predstavleno akademikom AN UkrSSR V.G. Bondarchukom [Bondarchuk, V.H.]...

ZARUTSKIY, K.M. [Zaruts'kyi, K.M.]

Mineralogical composition of the Buchak continental sediments of the right-bank area of the middle Dnieper. Dop. AN URSR no.11:1510-1512 '65. (MIRA 18:12)

1. Institut geologicheskikh nauk AN UkrSSR.

L 45665-66 EWT(m)/T UR/0080/66/039/007/1475/1481 SOURCE CODE: AP6025461 ACC NR 36 B AUTHOR: Zarubitskiy, C. G. ORG: Institute of General and Inorganic Chemistry, AN UkrSSR (Institut obschey i neorganicheskoy khimii AN UkrSSR) TITLE: Anodic polarization and potential vs time dependence SOURCE: Zhurnal prikladnoy khimii, v. 39, no. 7, 1966, 1475-1481 TOPIC TAGS: anodic oxidation, electrode potential, metal coating, metal oxidation, corrosion protection, corrosion ABSTRACT: Anodic polarization and electrode potential vs time dependence (0-200 minutes) was studied for several metals in liquid and solid state in molten sodium hydroxide at 340 ± 2°C. For W, Mo, and Cd, the electrode potential was found to reach a constant level rapidly and then remain constant with time. For Pb, Bi, and Cu, the electrode potential was found to reach a constant level slowly. Such metals as Ag, An, Ft, Fe, Ni, Ta, Nb, and Zr were found to be air-oxygen electrodes. At 340°C in molten NaOH, the following electrochemical order of metals was established: W, Mo; Cd, Pb, Bi, Cu, Ag, An, Pt, Fe, Ni, Ta, Nb, and Zr. The eathors thank Yu. K. Delimarkiy for valuable advice and instructions given during the investigation. Orig. art. has: 9 figures. OTH REF: 012 ORIG REF: 012/ SUBH DATE: 22Jun64/ SUB CODE: 07/ 541.13 UDC: Card 1/1

GRACH'YAN, A.N.; ZARUTSKIY, S.A.; STEPANOVA, A.I.; ZUBEKHIN, A.P.;

DYADISHCHEV, W.I.

Increasing the whiteness of cement clinker. TSement 28 no.1:11
Je-F '62. (Cement clinkers)

VAYNBERG, D.V. (Klyev); ZARUTSKIY, V.A. [Zaruts'kyi, V.O.] (Klyev);
ITEMBERG, B.Z. (Klyev)

Stressed state of cylindrical shells reinforced with ribs. Prykl.
mekh. 6 no.4:375-384 '60.

1. Institut stroitel'noy mekhaniki AN USSR.
(Klastic plates and shells)

10.6000 also 1327, 1103

8/198/61/007/005/005/015 D274/D303

AUTHOR:

Zaruts kyy, V.O. (Kyyiv)

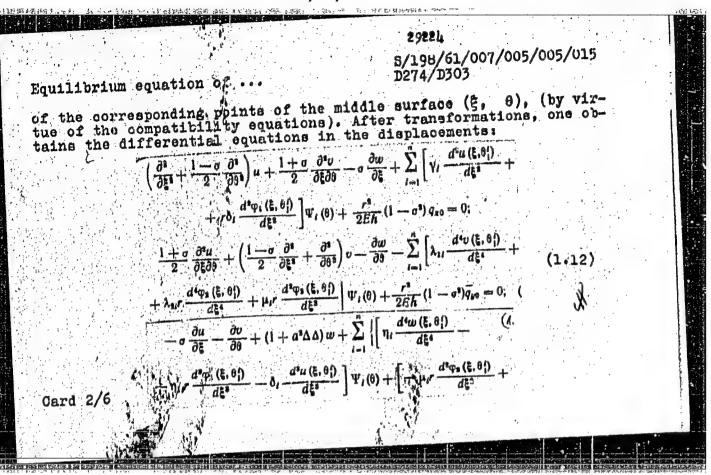
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Equilibrium equations of stiffened cylindrical shells

their approximate solution

PERIODICAL: Prykladnaya mekhanika, v. 7, no. 5, 1961, 503 - 510

The differential equations of equilibrium of stiffened cylindrical shells are derived, the width of the ribs (stringers) being taken into account. The obtained system of differential equations with variable coefficients is reduced to a system of ordinary differential equations with constant coefficients. A cylindrical shell, stiffened by stringers, is considered under arbitrary surface—and edge loads. It is assumed that the Kirchhoff-Love hypothesis applies to the shell, and that of plane sections — to the stringers. The components q of the external surface load, applied to the middle surface of the shell, are expressed in terms of the stresses bet-ween shell and stringers at their surface of contact. The displacements u, v, w of the stringers are expressed by the displacements Card 1/6.



29224 S/198/61/007/005/005/015 D274/D303

Equilibrium equation of ..

$$+ \lambda_{44} \frac{\left(d^4 v\left(\xi,\theta\right)\right)}{d\xi^4} + \lambda_{24} r \frac{d^4 \varphi_2\left(\xi,\theta\right)}{d\xi^4} \left[\frac{d\Psi_1\left(\theta\right)}{d\theta} \right] = \frac{r^2}{2Eh} \left(1 - \sigma^2\right) \overline{q_{10}}, \qquad (1.12)$$

where φ , γ , δ , λ , μ , Ψ , η , are given by expressions. If $\theta_0^1 = 0$, Eqs. (1.12) reduce to the analogous equations of the theory of stiffened shells with stringers of zero width. As an example, a cylindrical shell with stringers is considered, under axisymmetric loading. The stringers are at equal distances and have the same loading. The stringers are at equal distances and have the same geometrical—and elastic characteristics. In this case, the stressed state of the shell has cyclic symmetry with angle $2\pi/n$. Hence the sought-for displacements can be expressed by infinite series:

ries;

$$u = \sum_{k=0}^{\infty} u_k(\xi) \cos kn\theta; \quad v = \sum_{k=1}^{\infty} v_k(\xi) \sin kn\theta; \quad w = \sum_{k=0}^{\infty} w_k(\xi) \cosh kn\theta.$$
(2.1)

The approximate solution of Eq. (1.12) is sought in the form Card 3/6

Equilibrium equation of $\frac{2922l_k}{5/198/61/007/005/005/015}$ $u_{k_i} = \sum_{k=0}^{n} u_{kk_i}(\xi) \cos kn\theta; \quad v_{k_i} = \sum_{k=1}^{n} v_{kk_i}(\xi) \sin kn\theta;$ $w_{k_i} = \sum_{k=0}^{n} w_{kk_i}(\xi) \cos kn\theta.$ $w_{k_i} = \sum_{k=0}^{n} w_{kk_i}(\xi) \cos kn\theta.$ The displacements u, v, w are imparted to the shell; these displacements are determined from the condition $\frac{237}{n}$ $(\vec{p}\vec{v}_{k_1}) rd\theta = 0$ where \vec{p} is the surface-load vector and u is determined from Eq. (2.2) This condition is satisfied if $\frac{2\pi}{n} \rho_{k} u_{k_i} d\theta = 0; \quad \int_{0}^{\infty} \rho_{k_i} u_{k_i} d\theta = 0.$ Card 4/6

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S/198/61/007/005/005/015 D274/D303

Equilibrium equation of ...

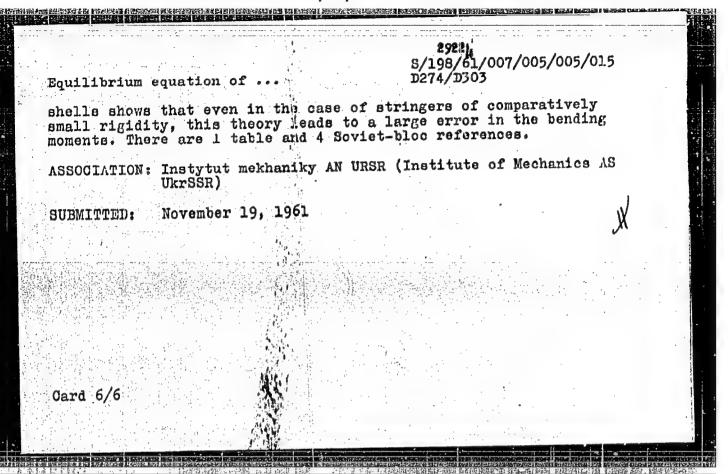
Substituting (2.2) in (2.4), one obtains, in turn, the conditions under which (2.4) is satisfied, viz.:

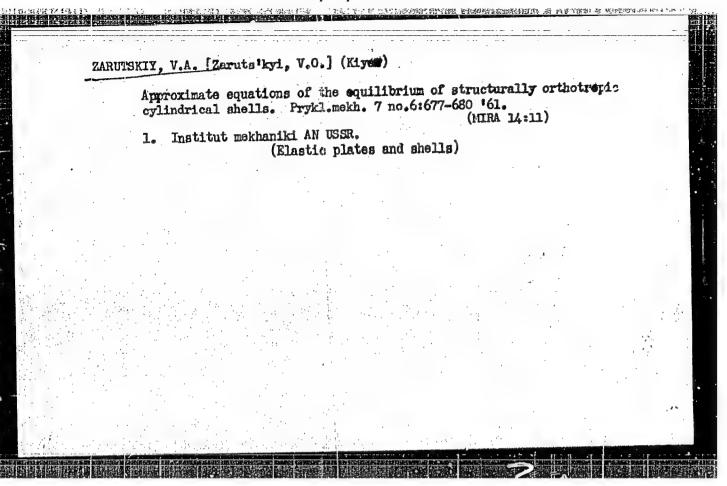
$$\int_{0}^{2\pi} \rho_{x} \cos kn\theta d\theta = 0; \qquad \int_{0}^{2\pi} \rho_{y} \sin kn\theta d\theta = 0; \qquad (2.5)$$

$$\int_{a}^{2\pi i} \rho_{x} \cos kn\theta \, d\theta = 0 \quad k = 0, 1, 2, \dots, k_{1}.$$

Thus, the system of three partial differential equations is reduced to $3k_1 + 2$ ordinary differential equations. The above method is an extension of L.V. Kantorovich's method for three variables, (Ref. 4: Priblizhenyye metody vysshego analize, GITTL, 1949). Further, a numerical example is considered. From this example it is evident numerical example is considered. From this example it is evident that in determining the bending moments, the width of the stringers that in determining the bending moments, the width of the stringers are of considerable importance. A comparison of the above computations with those based on the theory of structural-orthotropic

Card 5/6





ZARUTSKIY VO.

37684 \$/198/62/008/003/004/008 D407/D301

O,700° AUTHOR:

Zaruts'kyy, V.O. (Kyyiv)

TITLE:

On calculating cylindrical shells, reinforced by

stringers

PERIODICAL: Prykladna mekhanika, v. 8, no. 3, 1962, 271 - 281

TEXT: A circular cylindrical shell is considered, reinforced by stringers which are equally spaced and have similar geometrical—and mechanical characteristics. The shell is subjected to cyclic symmetrical loads with periodic 2N/n (n being the number of stringers). The equilibrium equation in the displacements is derived. The boundary conditions are obtained by means of the principle of virtual displacements. First, the case of a shell subjected to a surface load, is considered. If the shell is rigidly supported at the ends, the solution of the equilibrium equation is obtained in the form of double trigonometric series; this constitutes a particular solution of the equilibrium equation which can be used for the determination of the general solution, i.e. of the stressed-strained state of a shell, loaded at the ends. In this case one obtains an infinite sys-

S/19a/62/008/003/004/008

On calculating cylindrical shells, ... D407/D301

tem of ordinary differential equations, which (in turn) yields a system of homogeneous algebraic equations; the latter system has a system of homogeneous algebraic equations; the latter system has a system of homogeneous algebraic equations; the latter system has a system of homogeneous algebraic equations of infinite order:

the algebraic equation of infinite order:

the algebraic equations; the latter system has a system has a system has a system of the solutions. Determination of the displacements reduces to solving Eq. (3.6) and to the finding of the arbitrary constants A, B and C (obtained from the boundaring of the arbitrary constants A, B and C (obtained from the boundaring of the arbitrary constants A, B and C (obtained from the boundaring of the arbitrary constants A, B and C (obtained from the boundaring of the arbitrary constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B and C (obtained from the boundary error constants A, B an

\$/198/62/008/003/004/008 On calculating cylindrical shells, ... 1407/2301

These conditions can be expressed by the inequality

 $e^2n^4 \gg 1$,

(3.13)

where a² = h²/3r² (2h being the wall thickness, and r - the radius of curvature of the middle surface of the wall). If condition (3.13) is satisfied, then the algebraic equations and the boundary conditions can be simplified. Further, the theory of structurally-orthotropic shells is used for calculating reinforced shells. A formula is derived which expresses the sufficient condition for the applicability of that theory for the latter purpose. A numerical example is given which shows that the approximate solution which is much simpler than the exact one, yields satisfactory results: the theory simpler than the exact one, yields satisfactory results; the theory of orthotropic shells, on the other hand, leads to large errors. There is 1 figure, 1 table and 2 Soviet-bloc references.

ASSOCIATION: Instytut mekhaniky AN URSR (Institute of Mechanics of

the AS UkrRSR)

SUBMITTED: February 9, 1962

Card 3/3

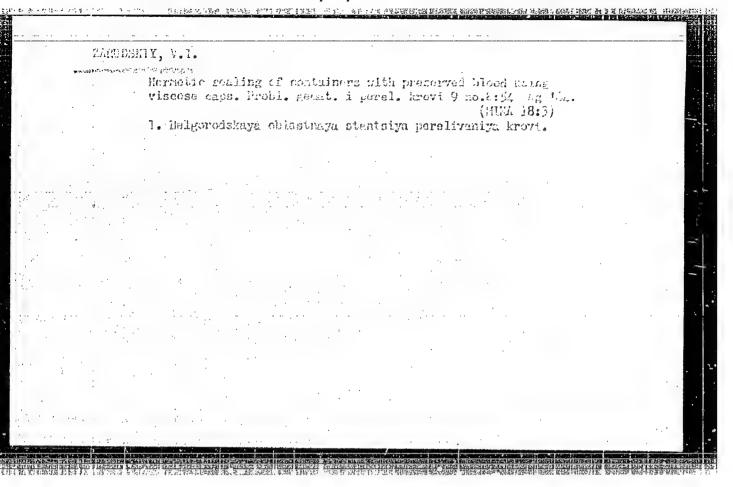
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Equilibrium equations for	0234/0308
The system of algebraic equat:	ions obtained in this way has a not-
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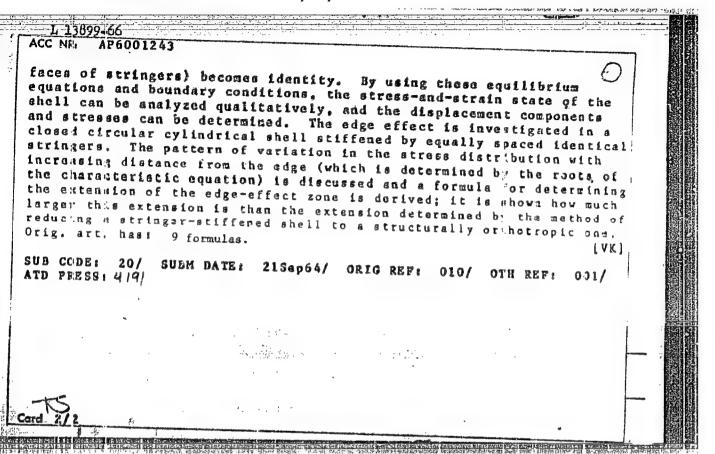
L_J3B99(200 __947(0)/EXT(m)/EXP(K)/EXA(0)/ETC(m)=0/EXF(W)/EXF(Y) __JJF(C) __131/HK AP6001243 (N) SOURCE CODE: UR/0198/65/001/011/0028/0038 ROHTUA : Zarutskiy, V. A. (Kiev) ORG: Institute of Mechanics, Academy of Sciences UkrSSR (Institut mckheniki Akademii nauk UkrSSR) TITLE: Equilibrium of stiffened cylindrical shells SOURCE: Prikladnaya mekhanika. v. 1. no. 11. 1965. 28-38 TOPIC TAGS: cylindrical shell, cylindrical shell equilibrium, stiffened shall, stiffened cylindrical shell edge effect, edge effect. enos ABSTRACT: A homogeneous system of integro-differential equations of equilibrium of longitudinally and laterally stiffened cylindrical shells is derived in terms of displacements, starting from their elastic-strain energy equations and compatibility conditions of the joint deformation of the skin-stiffener system, under the assumption that the theory of thin clastic shells is applicable to the skin, and the formulas of the strength of materials to the stiffeners. The shelks are subjected to arbitrary surface and face-edge loading. The boundary conditions are formulated as conditions under which a variational equilibrium equation (in terms of external forces acting on

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Card 1/2

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CIA-RDP86-00513R001963910002-0



BOURGE CODE: UR/0258/65/005/005/0895/0906 AUTHOR: Zerutskiy, V. A. (Kiev) ORG: none TITLE: On designing stiffened cylindrical shells SOURCE: Inzhenernyy zhurnal, v. 5, no. 5, 1965, 895-906 TOPIC TAGS: shell, cylindrical shell, stiffened cylindrical shell, stronger stiffened shell, longitudinally stiffened shell ABSTRACT: The stress and strain distribution in a closed circular cylindrical shell stiffened by n equally spaced stringers having identical geometric and mechanical characteristics is considered. The shell is subjected to cyclically (period $2\pi/a^{\frac{1}{2}}$ symmetric loadings applied at the faces of the shell; the states of stress and strain possess the same cyclic symmetry. The derivation of equilibrium equations and boundary conditions (in which a discrete spacing of stringers is taken into account) by using the principle of virtual displacements is based on the following assumptions 1) the theory of thin elastic shells !considering a high index of variation' is a; plicable to the shell skin; 2) the strength-of-materials formulas are applicable to the stringers; and 3) the coupling of displacements of the stringer axes with displacements of corresponding points at the middle surface of the skin is expressed by given equations. The solution of the equilibrium equation satisfying the boundary **Card** 1/2 624.074

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conditions is sought in the form of a simple trigonometric series which leads to the solution of an infinite system of linear algebraic equations. The effect of the edge loading on the state of atress in the skin (membrane stresses combined with bending stresses having an "edge-effect" character in the vicinity of stringers is anaproblem) is given and the formulas for determining the displacement components of the problem) is given and the formulas for determining the displacement components of the triase. As an example, expressions are derived for the deflection of a semi-infinite cylindrical shell stiffened by stringers and subjected to bending moments continuous, pression shows that the formulas of the theory of structurally orthotropic shells can be used in calculating the deflections of stiffened shells with certain geometric che shell is also determined. Orig. art. has: I figure, 29 formulas, and I table. [VK] UB CODE: AS/ SUBM DATE: O3May63/ ORIG REF: O11/ OTH REF: O00/ AND PRESS: 4/125
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L 39771-66 EWI(d)/EWI(m)/EWP(w)/EWP(v)/EWP(k)/EWA(h)/EIC(m)-6IJP(c) AP6014214 ACC INRI SOURCE CODE: UR/0198/66/002/004/0017/0025 (AL. AUTHOR: Zarutskiy, V. A. (Kiev) Institute of Mechanics. AN Ukrssk (Institut mekhaniki AN UkrssR) TITLE: Design of stiffened cylindrical shells, under arbitrary loads SOURCE: Prikladnaya mekhanika, v. 2, no. 4, 1966, 17-25 TOPIC TAGS: cylindric shall, stiffened shall, shall design ABSTRACT: An expansion of previous qualitative analyses by the author on stress and strain; distributions in closed circular cylindrical shells stiffened by equidistant identical stringers is presented, starting with the particular solution of a previously derived inhomogeneous system of differential equilibrium equations in displacements with associated boundary conditions; the loads acting on the surface and at the ends of the shell are arbitrary. The obtained displacements are presented as a sum of: a) displacements in a plain infinite shell; b) displacements in a plain shell of finite length; and c) displacements depending on the stiffness of stringers. The general solution of a homogeneous system of differential equilibrium equations in displacements is also given, and it is shown that the final solution of the Card 1./2

ACC NR. AP6014214

problem can be obtained by using both particular and general solutions, and the boundary conditions for the stress and strain analyses of circular shells under a given type of loading. The qualitative results obtained show: 1) the dependence of the states of stress and strain in stiffened shells on the rigidity of stringers in tension, on their flexural rigidity in radial and tengential planes, and on torsional rigidity; 2) the length and character of the odge-effect zone caused by the end loads; and 3) the possibility of applying the equations of the theory of structurally orthotropic shells to the design of stiffened shells under arbitrary loading; a criterional formula is derived which represents the necessary and sufficient condition for such an application. Orig. art. has: 21 formulas. [VK]

SUB CODE: 20/ SUBM DATE: 12Ju165/ ORIG REF: 007/ ATD PRESS:42444

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ACC NR. AP6021546 (A) SOURCE CODE: UR/0198/66/002/006/0055/0062

AUTHOR: Zarutskiy, V. A. (Klev)

30 3

ORG: Institute of Mechanics, AN UKrSSR (Institut mekhaniki AN UKrSSR)

TITLE: Use of double trigonometric series for designing finned cylindrical shells

SOURCE: Prikladnaya mekhanika, v. 2, no. 6, 1966, 55-62

TOPIC TAGS: cylindric shell structure, shell design, shell stability

ABSTRACT: Double trigonometric series are used to determine the stress-strain state of circular closed cylindrical shells reinforced by discretely distributed fins and subjected to the effect of cyclically symmetric loads. It is shown that as a result of using double trigonometric series it is possible to solve the problem of determining the stress-strain state of finned cylindrical shells and to calculate the forces, moments, and displacements with a preassigned accuracy. The calculation of the shells can be reduced to a solution of quasi-regular infinite systems of linear algebraic equations. Orig. art. has: 16 equations.

SUB CODE: 13/ SUBM DATE: 27Aug65/ ORIG REF: 007

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ZARUTSKIY, V.V.; ARAKELYAN, V.G.; OSTROVSKIY, S.A.; GOLOVKIN, G.V.

Improving the sensitivity of the detector in a Kh.T.-2M device. Zav. lab. 30 no.10:1286 '64. (MIRA 18:4)

1. Institut organicheskoy khimii imeni Zelinskogo AN SSSR.

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GOLOVKIN, G.V.; PRYANISHNIKOVA, M.A.; KONONOV, N.F.; PLATE, A.F.; ZARUTSKIY, V.V.

Preparation of bicyclo[2,2,1]hepta-2,5-diene; effect of the nature of phlegmatizer, temperature, pressure, and cyclopentadiene feed rate. Izv. AN SSSR.Ser.khim. no.10:1850-1855 165.

(MIRA 18:10)

1. Institut organicheskoy khimii im. N.D.Zelinskogo AN SSSR.

KASATKIN, A.G.; DYTNERSKIY, Yu.I.; ZARUTSKIY, V.V.; PETROV, G.G.; GORYACHEVA, R.V.

Separation of liquid homogeneous systems by means of polymeric films. Trudy FKHTI no.40:156-160 '63.

(MIRA 18:12)

LEPESHINSKAYA, V.N.; ZARUTSKIY, Yo.M.

Penstration of ions of covering alkali metals details

Penetration of ions of certain alkali metals into copper and silver. Izv. AN SSSR. Ser. fiz. 28 no.8:1390-1394 Ag '64 (MIRA 17:8)

1. Leningradskiy politekhnicheskiy institut.

ZARUTSKIY, Yu. F.

Cand Tech Sci - (diss) "Grid current, calculations, and design for electrometric tubes." Moscow, 1961. 15 pp; (Ministry of Higher and Secondary Specialist Education RSFSR, Moscow Order of Lenin Power Inst); 150 copies; free; (KL, 5-61 sup, 189)

ZAKUTSKIY V. O

32561

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S/198/61/007/006/008/008 D299/D301

AUTHOR:

Zaruts'kyy, V. C. (Kyyiv)

TITLE:

Approximate equilibrium equations of structurally orthotropic cylindrical shells

PERIODICAL:

Prykladna mekhanika, v. 7, no. 6, 1961, 677-680

TEXT: A thin shell is considered, stiffened by a large number of longitudinal ribs. An approximate system of equations is derived, based on V. Z. Vlasov's engineering theory of cylindrical shells. The stress function is introduced by means of the formula

$$T_1 = \frac{1}{r^2} \frac{\partial^2 \varphi}{\partial \theta^2} ; \quad T_2 = \frac{1}{r^2} \frac{\partial^2 \varphi}{\partial \xi^2} ; \quad S_1 = -\frac{1}{r^2} \frac{\partial^2 \varphi}{\partial \xi \partial \theta}$$
 (5)

A system of equations for determining the unknown functions \(\textit{f} \) and \(\text{w is obtained:} \)

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Approximate equilibrium equations ...

$$\frac{\partial^{2} \varphi}{\partial \xi^{2}} - \frac{\delta}{1 + \gamma - \sigma^{2}} \frac{\partial^{3}}{\partial \xi^{2}} \left[\frac{\partial^{2} \varphi}{\partial \theta^{3}} - \sigma \frac{\partial^{2} \varphi}{\partial \xi^{2}} \right] - \frac{2Eh^{2}}{3(1 - \sigma^{2})r} \left\{ \left[1 + \lambda \right] - \frac{\delta^{3}}{a^{2}(1 + \gamma - \sigma^{2})} \right] \frac{\partial^{4} w}{\partial \xi^{4}} + 2 \frac{\partial^{4} w}{\partial \xi^{2} \partial \theta^{3}} + \frac{\partial^{4} w}{\partial \theta^{4}} = r^{3}Z, \tag{6}$$

$$\frac{\partial^{2} w}{\partial \xi^{2}} - \frac{\delta}{1 + \gamma - \sigma^{2}} \frac{\partial^{3}}{\partial \xi^{2}} \left[\frac{\partial^{2} w}{\partial \theta^{3}} - \sigma \frac{\partial^{2} w}{\partial \xi^{2}} \right] + \frac{1 - \sigma^{2}}{2Ehr(1 + \gamma - \sigma^{2})} \times \left[(1 + \gamma) \frac{\partial^{4} \varphi}{\partial \xi^{4}} + 2 \left(1 + \frac{\gamma}{1 - \sigma} \right) \frac{\partial^{4} \varphi}{\partial \xi^{2} \partial \theta^{2}} + \frac{\partial^{4} \varphi}{\partial \theta^{4}} \right] = 0.$$

$$\gamma = \frac{E_{1} \vec{F}_{1}}{2Eh} (1 - \sigma^{2}); \quad \delta = \frac{E_{1} \vec{A}_{1}}{2Ehr} (1 - \sigma^{2}); \quad \lambda = \frac{3E_{1} \vec{I}_{1}}{2Eh^{2}} (1 - \sigma^{2}),$$

 F_1 , A_1 and I_1 being (respectively) the area, static moment and moment of inertia of the rib cross-section with respect to the θ -Card 2/5

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D299/D301

Approximate equilibrium equations ...

axis. Eq. (6) is solved separately for each m, the load being expressed in the form of trigonometric series in θ , for example Z =

$$= \sum_{m=0}^{\infty} Z_m(\zeta) \cos m\theta; \quad \varphi_{\hat{m}} \text{ and } w_m \text{ are sought in the form}$$

$$\varphi_{\rm m} = \Lambda_{\rm m} e^{r_{\rm m} \xi} \cos m\theta; \ w_{\rm m} = B_{\rm m} e^{r_{\rm m} \xi} \cos m\theta$$
 (7)

Substituting Eq. (7) in Eq. (6), one obtains the characteristic equation

$$c_{1m}r_{m}^{8} - c_{2m}r_{m}^{6} + c_{3m}r_{m}^{4} - c_{4m}r_{m}^{2} + c_{5m} = 0$$
 (8)

where

Card 3/5

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Approximate equilibrium equation: ...

$$c_{1m} = (1+\gamma)(1+\lambda) - \frac{\delta^{2}}{a^{2}};$$

$$c_{2m} = \frac{4m^{2} + \frac{2m^{2}}{1-\sigma} \left[\gamma(2-\sigma) - \frac{\delta^{2}}{a^{2}} + \lambda(1+\gamma-\sigma) \right] + \frac{2\sigma\delta}{a^{2}}; \qquad (9)$$

$$c_{3m} = \frac{1+\gamma-\sigma^{2}}{a^{2}} + 6m^{4} + m^{4} \left[\lambda + \frac{5-\sigma}{1-\sigma} \gamma \right] - 2m^{2} \frac{\delta}{a^{2}};$$

$$c_{4m} = 4m^{4} \left[1 + \frac{\gamma}{2(1-\sigma)} \right]; c_{8m} = m^{4}.$$

A comparison between the coefficients (9) of Eq. (8) and the coefficients obtained on the basis of the exact theory shows that by using the approximate equations, the error does not exceed $1/m^2$. This leads to the conclusion that the error in determining the

Card 4/5

 Approximate equilibrium equations ...

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stressed state of the shell by means of Eqs. (6) and (7) is of the same order $(1/m^2)$. An analysis of Eq. (8) shows that the solution of Eqs. (9) can be simplified, as well as the characteristic equation; thereby V. Z. Vlasov's equation for the semi-membrane state of shells is obtained. For values of $a^2m^4\lambda\gg 1$, the characteristic equation degenerates: Thereby the equations corresponding to the degenerate state of shells are obtained. The use of Eq. (6) leads to a considerable simplification in analysis of the stressed state of shells. Analogous equations can also be obtained for shallow shells. There are 4 Soviet-bloc references.

ASSOCIATION: Instytut mekhaniky AN URSR (Institute of Mechanics AS UkrRSR)

SUBMITTED: August 1, 1960

Uard 5/5

SHOSTAYOVSKIY, M.F.; CHEKULAYEVA, I.A.; KONONOV, N.F.; ZARUTSKIY, V.V.; OSTROVSKIY, S.A.; ARAKELYAN, V.G.

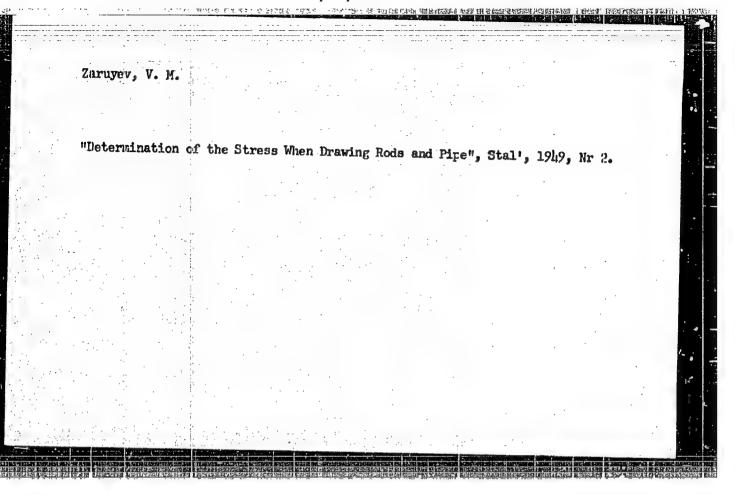
Triethanolamine vinylation reaction. Izv, AN SSSR. Ser. khim. no.4: 698-701 165. (MIRA 18:5)

1. Institut organicheskov khimii im. N.D.Zelinskogo AN SSSR.

ACC NR. A.T6004862 SOURCE CODE: UR/2563/65/000/255/0166/0171 AUTHOR: Berezin, G. N.; Zarutskiy, Ye. M.; Lepeshinskaya, V. N. ORG: none & TITLE: Effect of cesium-ion bombardment upon the secondary-emission properties of alloy-type magnesium-oxide and beryllium-oxide emitters SOURCE: Leningrad. Politekhnicheskiy inst'tut. Trudy, no. 255, 1965. Radiovlek ronika (Radio electronics), 166-171 TOPIC TAGS: secondary emission, photomultiplier, ion bombardment, magnesium oxide, beryllium compound, cesium, electron emission ABSTRACT: Important for understanding the photoniultiplier-fatigue phenomenon, an experimental investigation was organized of the effect of cesium-ion bombardment upon the secondary-electron-emission factor σ of magnesium-oxide and berylliumoxide films that are formed as a result of activation of CuAlMg and CuAlBe alloys. Experimental curves of $\sigma(E_{\rm D})$, $\sigma_{\rm max}$ / $\sigma_{\rm o}$ max vs. Ei and Ii for 10-, 30-, and 60min bombardment in a 10-6-torr vacuum are shown; Ei is the ion energy and Ii is the density of the ion beam. The fall-off of the $\sigma_{max}/\sigma_{0,max}$ curve depends on the

ACC NR. AT6004862	0
Two experimental curves of the	than on their energies; this result is in agreement Appl. Phys., 1959, v. 30, no. 7. pp. 1086-1100). ion-electron emission factor $\mathcal{S}(E_1)$ and the ion-ion \mathcal{S} increases linearly and K is practically has: 5 figures.
SUB CODE: 20, 09 / SUPM DA	TE: none / ORIG REF: 003 / OTH REF: 003
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Card 2/2 ~	

Practical training. Grazhd.av. 18 no.8:9 Ag '61. (MIRA 14:8) 1. Komandir eskadril'i Privolzhskogo upravleniya Grazhdanskogo vozdushnogo flota. (Flight training)	1. Komandir eskadril i Privolzhskogo upravleniy Grazhdanskogo vozdushnogo flota.		V., pilot
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			(Flight training)



ZARUYEV, V.M., dots.

Applying the law of least energy to determine the coefficient of dreft in rolling with nonuniform reduction, Obr. net.darl. no3: 27-32 '54. (MIRA '12:10)'

1. Donetskiy industrial nyy institut. (Rolling (Metalwork))

Zaruyev, V. M.

"Determination of the Force of Friction of Metal on the Walls of the Cylindrical Part of the Die in Wire Drawing", Metiznoye Proizvodstvo, Sbornik Statey, Vol I, Metallurgizdat, Moscow, 1956.

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SOV/137-57-11-22402

Translation from: Referativnyy zhurnal, Metallurgiya, 1957, Nr 11, p 253 (USSR)

AUTHORS: Zaruyev, V.M., Prourzin, V.K.

TITLE:

The Mechanical Properties of Nr 55S2 Steel at Elevated Tempera-

tures (Mekhanicheskiye svoystva stali 55S2 pri vysokikh

temperaturakh)

PERIODICAL: Tr. Donetsk. industr. in-ta, 1957, Vol 19, pp 5-7

ABSTRACT:

The effect of test temperatures of from 20 to 1100°C upon b. 5, and of Nr 55S2 steel is investigated to determine the optimum temperature for the end of the rolling operation. The specimens were first oil-hardened from 860° and tempered at 400° for 1 hour. It is found that in this case the 5 of Nr 55S2 steel practically does not change up to 500° and then drops sharply. In the 820-900° test-temperature interval it is found that the decline in 5 ceases, this being related to phase recrystallization and change in grain size. It is recommended that the temperature at the end of rolling and forging be held at >950°.

N. K.

Card 1/1

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TOVPENETS, Ya.S.; ZARUYEV, V.M.; GONCHARENKO, N.I.; JABIY, A.S.

Effect of heat treatment over the heating needed for volling on the mechanical proporties of mine rails. Izv.vys.ucheb.zav.; met. no.4:145-152 '60. (MIRA 73:4)

1. Donetskiy industrial'nyy institut. (Railroads--Rails) (Steel--Heat treatment)

ZARUYEV, V.H.

124-58-6-7225

Translation from: Referativnyy zhurnal, Mekhanika, 1958, Nr 6, p 127 (USSR)

AUTHORS: Zaruyev, V.M., Prourzin, V.K.

TITLE: The Mechanical Properties of Steel 5552 at Elevated Temperatures

(Mekhanicheskiye svoystva stali 55S2 pri vysokikh temperaturakh)

PERIODICAL: Tr. Donetsk. industr. in-ta, 1957, Vol 19, pp 5-7

ABSTRACT: Results are given of an investigation made of the strength and

ductility of steel 55S2 at temperatures up to 1100°C.

N.M. Dubrovin

1. Steel--Mechanical properties 2. Steel--Temperature factors

Card 1/1

*** ***********************************	ZARJYEV	V.M., dots	ent.		**************************************				***************************************
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Subject

USSR/Aeronautics - Aircraft

AID P - 5520

Card 1/1

Pub. 58 - 11/17

Author

Zarva, B.

Title

Aviation without airfields

Periodical

Kryl. rod., 2, 20-22, F 1957

Abstract

A cursory review of the current attempts by Western airplane constructors to build aircraft capable of taking off and landing in absence of runways. The author goes over a number of new (chiefly American) models of such aircraft, showing the characteristic traits of their design. The article is said to be based on information gathered from foreign publications.

12 designs.

Institution:

None

Submitted

No date